



2 **Effective Stress Change and Cyclic Resistance of Saturated Sands**
3 **Under Uniform and Irregular Cyclic Shears**

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7 **Abstract** In this study, two marine sands collected from
8 Vietnam (Nam O sand) and Japan (Toyoura sand) with
9 similar grain size were tested under undrained uniform and
10 irregular cyclic shears and the effective stress change and
11 liquefaction resistance of the soils were then observed for
12 different cyclic shear conditions. For the uniform cyclic
13 shear, the tests were carried out with various cyclic shear
14 directions, different number of cycles (n), and a wide range
15 of shear strain amplitudes (γ). Meanwhile for the irregular
16 one, the two-directional cyclic shear tests were performed
17 with different amplitudes of maximum shear strain (γ_{\max}).
18 It is shown from the experimental results that firstly, the
19 threshold number of cycles (n_{tp}) and cumulative shear
20 strain (G^*_{tp}) for effective stress reduction in saturated
21 specimen at $D_r = 50 \pm 5\%$ of Nam O sand are about n_{tp}
22 $= 0.1\text{--}0.7$ cycle and $G^*_{tp} = 0.1\%\text{--}0.5\%$. For specimen at
23 $D_r = 70 \pm 3\%$ of Toyoura sand, values of n_{tp} are about
24 $0.03\text{--}0.3$ cycle while those of G^*_{tp} is constant at 0.1% .
25 Secondly, based on relationships between the cumulative
26 shear strain G^* and γ at the occurrence of liquefaction, the
27 threshold cumulative shear strain for liquefaction was
28 obtained as $G^*_{tfU} = 15\%$ and $G^*_{tfM} = 11\%$ for Nam O
29 sand and as $G^*_{tfU} = 24\%$ and $G^*_{tfM} = 19\%$ for Toyoura
30 sand under uni-directional and two-directional cyclic
31 shears, respectively. Thirdly, the results of G^*_{tp} and G^*_{tfM}
32 obtained from uniform cyclic shear were applied to the
33 earthquake-induced irregular cyclic shears, and practical

applicability was confirmed for different amplitudes of the 34
maximum shear strain. 35

Keywords Cyclic shear · Effective stress · 36
Granular material · Liquefaction 37
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Introduction 39

When a saturated soil layers are subjected to cyclic shear 40
under undrained condition, the pore water pressure is 41
produced and accumulated. When sandy soil layers with 42
lower relative density are subjected to strong cyclic shears, 43
the pore water pressure rapidly increases and the initial 44
liquefaction of the soils is often confirmed [1]. As the time 45
proceeds after cyclic loading, the dissipation of the cyclic 46
shear-induced pore water pressure results in the recom- 47
pression of the soil layer, then the vertical settlement would 48
be observed at the ground surface. Since sandy soils are 49
easily liquefied under strong cyclic loading such as during 50
earthquakes, the liquefaction resistance and the post-liq- 51
uefaction settlement have been studied intensively on dif- 52
ferent types of sand with various testing conditions [2–10]. 53
By using the triaxial cyclic shear tests under undrained 54
condition, Tatsuoka et al. [11] indicated that the shear 55
strength of Toyoura sand increases in proportion to the 56
relative density (D_r) and that the cyclic shear resistance of 57
the sand increases quickly when $D_r > 70\%$. Based on a 58
combination of cyclic simple shear tests and triaxial cyclic 59
shear tests on Fraser Delta sand, Vaid & Sivathayalan [12] 60
indicated that the cyclic shear resistance of the sand 61
increases with D_r for various conditions of lateral stress 62
meanwhile for loose density, the influence of lateral stress 63
condition becomes negligible. By using the multi-direc- 64
tional shaking table, Pyke et al. [6] concluded that the 65

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