

# USING SONO-ELECTROCHEMICAL PROCESS FOR DECOLORIZATION AND REMOVAL COD OF DISPERSE-YELLOW-7 DYE IN AQUEOUS SOLUTIONS

**Abstract.** The performance of using a sono-electrochemical process for decolorization and removal COD (*chemical oxygen demand*) of disperse-yellow-7 (DY7, 4-[4-(Phenylazo)phenylazo]-*o*-cresol) in aqueous solutions was investigated in different concentrations electrolytes of NaCl and CaCl<sub>2</sub> (0.02, 0.05, 0.1, and 0.2 mol/L), treatment time and DY7 concentration. The combination of electrochemical (EC) and ultrasonic (US) was called the sono-electrochemical (EC\_US) process, and it showed the highest treatment DY7 efficiency in comparison with applying EC or US treatment alone (EC\_US > EC > US). Using CaCl<sub>2</sub> electrolytes had a higher decolor capacity than NaCl electrolytes in the same concentration. At the dose of DY7: 25 ppm, the EC\_US method (*NaCl or CaCl<sub>2</sub> 0.1 – 0.2 mol/L, frequency 20 kHz, electrodes of TiO<sub>2</sub> and RuO<sub>2</sub>-IrO<sub>2</sub>-TiO<sub>2</sub>*) was totally removal of DY7\_25 ppm in aqueous solutions (100% color and 100% COD) within 45 min treatment. This could be a valuable alternative treatment method applying for dyeing wastewater or other refractory organic compounds contained in wastewater.

**Keywords:** ultrasound, electrochemical, sono-electrochemical, disperse yellow 7

## 1. Introduction

Textile industry causes considerably higher impacts on water pollution by discharging their effluents into various receiving bodies including ponds, rivers, and other public sewers. Major pollutants loaded from the textile industries are from several of their wet-processing operations like scouring, bleaching, mercerizing, and dyeing [1]. Among these processes, the dyeing process normally uses a large amount of water for dyeing, fixing, and washing processes. Thus, textile wastewater possesses a high COD value, a large amount of suspended solids, broadly fluctuating pH, strong color, high temperature, and low biodegradability caused by varying contaminants within the water environment [2]. Whereas most azo dyes are carcinogenic, other compounds such as aromatic amines must undergo oxidation to form more toxic by-products [2]. Therefore, the removal of azo dyes and other refractory organic contaminants in wastewater has attained much attention in terms of both academic and industrial interest [3-10].

Despite the fact that different biological and physical techniques have been effectively used in the remediation of organic contaminants, these methods have their own advantages and disadvantages. The majority of physical techniques, for example, reverse osmosis, adsorption, and flocculation are capable of transferring primary contaminants into secondary by-products, which results in different environmental issues [2]. Biological remediation methods face significant disadvantages, such as the creation of a large amount of sludge and poor removal efficiency of refractory organic pollutants [2]. Hence, the focus on advanced oxidation processes (AOPs) to overcome the disadvantages of some conventional remediation processes have attached many researchers. The most commonly used AOPs for the remediation of dyeing wastewater are used alone or combining these processes: Fenton-based oxidation [11], ozonation, electro-oxidation [12], and sono-electrochemical (EC\_US) [4-10]. Recently, the EC\_US technique has been

42 developed as a green chemistry process that involves the integration of electrochemical (EC) and  
43 ultrasound (US) processes for the degradation of a broad range of organic contaminants [13, 14].  
44 Some reviews of the treatment of dyes in aqueous solutions by sono-electrochemical methods are  
45 revealed in Table 1.

46 In sonochemistry, US can be divided into two classes, high frequency (2–10 MHz) that are mostly  
47 used in the medical field, and low frequency (20 kHz–2 MHz), where cavitation is produced in  
48 liquids and can be used to influence chemical reactions and chemical processes [13]. When a fluid  
49 is exposed to low-frequency US, the liquid “cavitates”. The cavitation bubbles produced as a result  
50 of exposure to ultrasound undergo extremely powerful collapse inside the fluid, producing “hot  
51 spots” of high energy [13]. In an EC process, chemical transformation takes place either  
52 spontaneously or non-spontaneously. In an electrolysis cell (non-spontaneously), an external EC  
53 potential/cell voltage or current is applied. EC reactions then occur at the interface between the  
54 electrolyte solution and the electrodes. The common reaction in electro-chemistry involves redox  
55 reactions [13]. The EC\_US process is based on a positive synergistic effect, where ultrasound  
56 waves with “hot spots” of high energy activate the surface of an electrode, promoting the rate of  
57 reaction and consequently, enhancing the efficiency of the electrode [13]. Turning to practice, the  
58 combination of US and EC processes in the degradation of COD and color of dyeing wastewater  
59 would be a good approach for enhanced treatment efficiency and minimizing waste. In this study,  
60 the sonolysis was performed at a frequency of 20 kHz. Two different supporting electrolytes,  
61 (NaCl, CaCl<sub>2</sub>) and a typical dye: disperse yellow 7 (DY7) were used to investigate the effects of  
62 electrolytes concentration, treatment time, DY7 concentration under EC\_US, EC, and US  
63 treatment conditions.

## 64 2. Materials and methods

### 65 2.1. Materials and reagents

66 The effects of US\_EC, EC, and US on decolorization and COD treatment of DY7 dye in aqueous  
67 solutions were studied. Details of the DY7 dye are shown in Table 1. The DY7 dye has maximum  
68 absorbance ( $\lambda_{max}$ ) at 430 nm. The treatment solution was prepared by dissolving DY7 dye at  
69 the dose of 100 ppm in distilled water and using it as the stock.

70 **Table 1.** Dye class, chemical structure, molecular weight, and concentration of DY7

Dye	IUPAC Name	Molecular Formula	Molecular Weight	Class structure	Maximum absorbance	Study concentration
			g/mol		nm	mg/L or ppm
DY7 (*)	4-[4- (Phenylazo)phenylazo] -o-cresol	C <sub>19</sub> H <sub>16</sub> N <sub>4</sub> O	316.4	Di-azo	430	10 – 50

71 (\*) The compound identifier (CID) is 22736

## 73 2.2. Experimental setup

### 74 2.2.1. Ultrasonic, electrochemical, and sono-electrochemical setup

75 In this study, a reactor cup of 250 mL working volume was used. The glass cell had a cylindrical  
76 body, containing electrodes of TiO<sub>2</sub> and RuO<sub>2</sub>-IrO<sub>2</sub>-TiO<sub>2</sub>.

77 The electrodes made from TiO<sub>2</sub> and RuO<sub>2</sub>-IrO<sub>2</sub>-TiO<sub>2</sub> offer several advantages, including high  
78 stability, durability, conductivity, potential range, catalytic activity, and low cost. These  
79 properties make them suitable for use in various electrochemical applications, including water  
80 treatment [15]. These electrodes have high stability and durability in various harsh chemical  
81 environments. They are resistant to corrosion and can withstand high temperatures and  
82 pressures, making them ideal for use in electrochemical processes that require long-term stability.  
83 These electrodes have high electrical conductivity, which makes them efficient in transferring  
84 charge between the electrode surface and the electrolyte solution. This results in faster reaction  
85 rates and higher current densities, leading to improved electrochemical performance. In addition,  
86 these electrodes have a wide potential range, high catalytic activity which means they can be used  
87 for a variety of electrochemical reactions. TiO<sub>2</sub> electrodes are relatively low cost compared to  
88 other electrode materials, such as platinum or gold. The combination of RuO<sub>2</sub> and IrO<sub>2</sub> provides  
89 a synergistic effect, where the two materials work together to enhance the catalytic activity. The  
90 addition of TiO<sub>2</sub> helps to improve the stability and durability of the electrode.

91 The voltage source applied to the electrode is a direct current power source with a voltage of 12  
92 volts (Figure 1). The electrodes had an effective electrode area of 7 cm<sup>2</sup> and an electrode gap of 4  
93 cm in the dyeing solution. The ultrasonic maximum power is 200 watts and the frequency is 20  
94 kHz (Tomy Seiko CO., Ltd, Japan), and the output nozzle hole area was 0.2 cm<sup>2</sup>. An ampere meter  
95 was connected to measure the electrical current (mA). In this study, the performance of three  
96 methods: ultrasonic (US), electrochemical (EC), and sono-electrochemical (EC\_US) in the  
97 treatment of DY7 was tested with the presence of different concentrations of electrolyte (pure  
98 salts: NaCl and CaCl<sub>2</sub>: 0.02, 0.05, 0.1, and 0.2 mol/L) during 60 minutes' treatment time. All  
99 experiments are triplicates.



100  
101 **Figure 1A.** ultrasonic, electrochemical, and sono-electrochemical experiments setup.

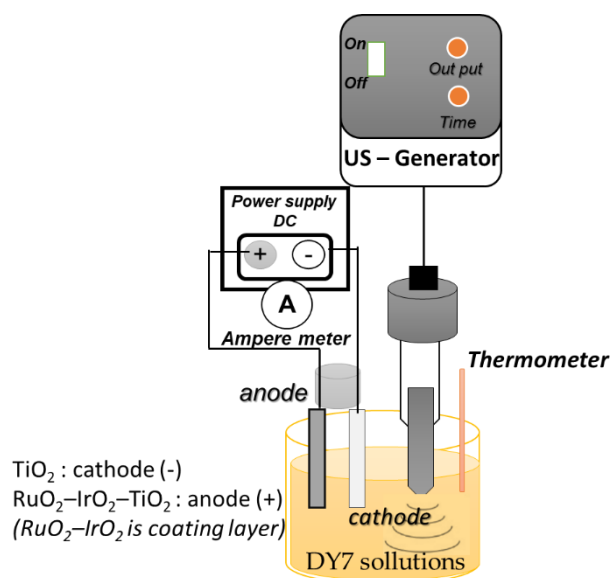


Figure 1B. Diagram of experiments setup

### 2.2.2. Color and COD analysis

The percentage of decolorization was determined according to the following equation:

$$\text{Decolorization (\%)} = [(A_0 - A_t) \times 100\%]/A_0 \quad (1)$$

Where:  $A_0$  is the absorbance value at 430 nm at the beginning (0 min).

$A_t$  is the absorbance value at 430 nm at the treatment time (t min, t: from 0 – 60 min).

The percentage of COD removal was determined according to the following equation:

$$\text{COD removal (\%)} = [(COD_0 - COD_t) \times 100\%]/COD_0 \quad (2)$$

Where:  $COD_0$  is the COD value at the beginning (0 min).

$COD_t$  is the COD at the treatment time (t min, t: from 0 – 60 min).

The COD values were analyzed following the standard method [16]. In this experiment, it was found that in the range COD of 0 – 90 mg/L, at 420 nm, the standard curve obtained is  $y = -0.0017x + 0.1998$ , and  $R^2 = 0.9968$ . Where: y is the absorbance value and x is the COD value.

## 3. Results and discussion

### 3.1. Relationship between DY7 concentration and COD or absorbance at 430 nm

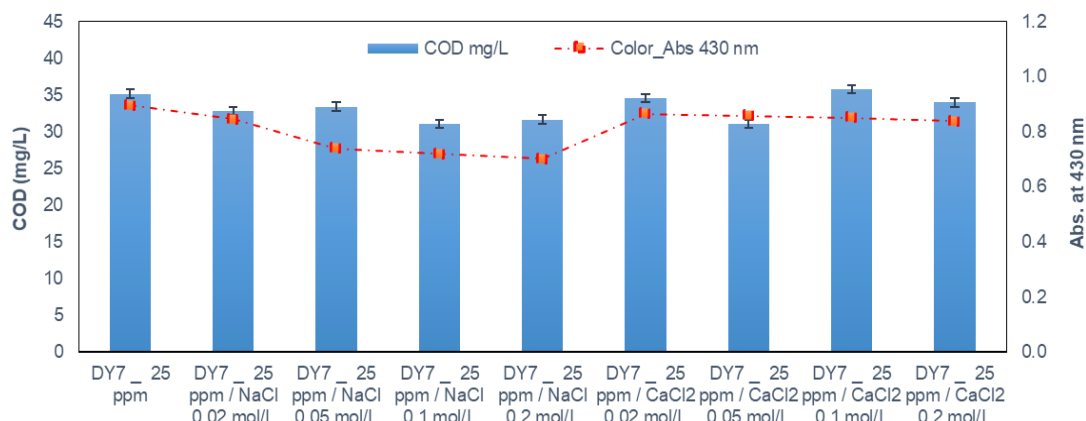
The Pearson correlation coefficient ( $R^2$ ) was calculated at 0.9998 and 0.9859 for relationships between the concentration of DY7 and COD, concentration of DY7 and absorbance at 430 nm, respectively. The data from Table 2 show that the DY7 concentration value increases, the COD value increases accordingly. As the concentration of DY7 increased from 5 ppm to 25 ppm, the ratio of COD and DY7 concentration was about  $1.5 \pm 0.1$  and the ratio of absorbance at 430 nm and DY7 concentration was  $0.035 \pm 0.001$ .

**Table 2.** Relationship between DY7 concentration and COD or absorbance at 430 nm

DY7 concentration (mg/L or ppm)	COD (mg/L)	Absorbance at 430 (nm)	COD: DY7 concentration	Absorbance at 430 nm : DY7 concentration
0	0	0.000		
5	8	0.173	1.60	0.035
10	15	0.350	1.50	0.035
25	35	0.896	1.40	0.036

### 125 3.2. Effect of ultrasonic power in the removal of DY7

126 At first, the COD and the absorbance at 430 nm of all input samples were analyzed and shown in  
 127 Figure 2. There is a small fluctuation of COD and absorbance at 430 nm of adding CaCl<sub>2</sub> or NaCl  
 128 into 25 ppm DY7 solutions. The effect of ultrasonic power in the treatment of DY7 was tested for  
 129 all of the samples (Figure 2) for 60 min. In fact, using only US treatment (20 KHz, 500 w/cm<sup>2</sup>) was  
 130 not effective in the removal of color, and COD of the DY7 dye in aqueous solution.



131

132 **Figure 2.** COD and absorbance at 430 nm values after adding CaCl<sub>2</sub> or NaCl to 25 ppm DY7

133

solutions

### 134 3.3. Effect of different supporting electrolytes on DY7 removal by electrochemical process

135 Supporting electrolytes play an important role in electrochemical processes because they allow  
 136 the flow of current through the solution and facilitate electrochemical phenomena such as  
 137 oxidation, reduction, and conduction. Specifically, the supporting electrolyte facilitated the  
 138 removal efficiency of color and COD in wastewater (Table 3 and Table 4). Under two supporting  
 139 electrolytes, the experimental results showed that CaCl<sub>2</sub> (Table 3) electrolytes had higher  
 140 efficiency than NaCl (Table 4). Under supporting 0.05 mol/L CaCl<sub>2</sub> electrolyte, the COD removal  
 141 efficiency was 70.3%, and the color removal efficiency was 65.6% after 60 min treatment time.

142

143 **Table 3.** Percentage removal COD and color of DY7<sub>25</sub> ppm in 0.05 mol/L CaCl<sub>2</sub> by EC process

Time, min	COD, mg/L	COD removal efficiency, %	Absorbance at 430 nm	Color removal efficiency, %	Electric current, mA
0	35.2	0.1	0.896	0	170
5	26.4	25.2	0.663	26	
10	23.4	33.5	0.428	52.2	
20	19.9	44	0.386	56.9	
30	14.6	58.6	0.324	63.8	
45	14	60.3	0.327	63.5	
60	10.5	70.3	0.308	65.6	230

144 **Table 4.** Percentage removal COD and color of DY7\_25 ppm in 0.05 mol/L NaCl by EC process

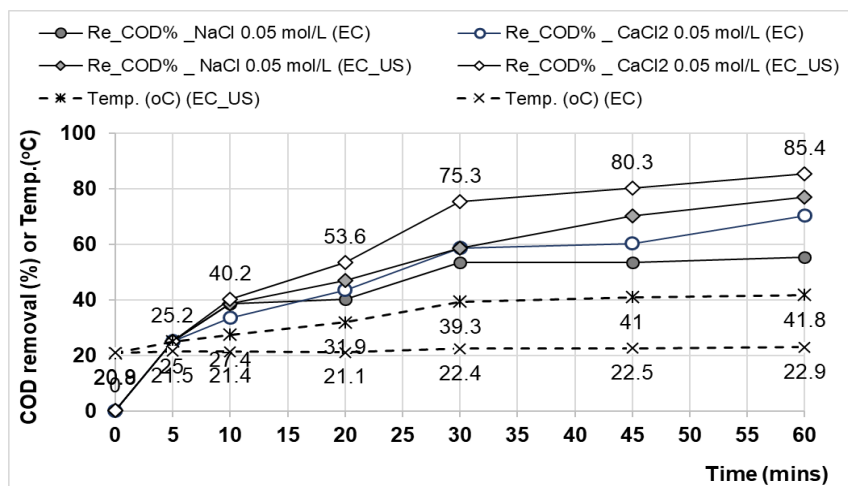
Time, min	COD, mg/L	COD removal efficiency, %	Absorbance at 430 nm	Color removal efficiency, %	Electric current, mA
0	35.2	0.1	0.896	0	100
5	26.4	25.2	0.732	18.3	
10	21.6	38.5	0.634	29.2	
20	21.1	40.2	0.594	33.7	
30	16.4	53.6	0.524	41.5	
45	16.4	53.6	0.478	46.7	
60	15.8	55.3	0.428	52.2	150

145 **3.4. Effect of electrolytes (NaCl and CaCl<sub>2</sub>) on DY7 removal by EC\_US process**

146 The efficiency of COD removal in 0.05 mol/L NaCl of the EC process showed that after 10, 30, and  
 147 60 minutes, the efficiency of COD removal increased by 38.5%, 53.6%, and 55.3%. (Table 4). In  
 148 0.05 mol/L CaCl<sub>2</sub> of the EC process showed that after 10, 30, and 60 minutes, the efficiency of COD  
 149 removal increased by 33.5%, 58.6%, and 70.3%. (Table 3). In 0.05 mol/L NaCl of the EC\_US process  
 150 showed that after 10, 30, and 60 minutes, the efficiency of COD removal increased by 38.5%,  
 151 58.6%, and 77%. Similarly, in 0.05 mol/L CaCl<sub>2</sub> of the EC\_US process showed that after 10, 30, and  
 152 60 minutes, the efficiency of COD removal increased by 40.2%, 75.3%, and 85.4%. The efficiency  
 153 of color removal was also well achieved under the EC\_US treatment process (Figure 3). Although  
 154 EC degradation is considered a clean process for removing organic contaminants, it has a few  
 155 drawbacks of low degradation efficiency and the electrode is passivated because of frequent  
 156 electrode fouling [13, 14]. The use of the EC\_US process can resolve the issues experienced using  
 157 EC processes alone [8]. In fact, after 60 min EC\_US process treatment time, the surface of  
 158 electrodes used in this study (TiO<sub>2</sub> and RuO<sub>2</sub>-IrO<sub>2</sub>-TiO<sub>2</sub>) is very clean. In addition, there was a  
 159 significant increase in temperature (°C) during the EC\_US treatment time (from 0 to 60 min). The  
 160 temperature of all EC\_US experiments was gradually increasing from 21.5 ± 1.0°C to 42.0 ± 1.0°C,  
 161 by contrast, there was a very small change in temperature in the EC treatment process (Figure 3).

162 The effect of EC\_US in the treatment of DY7\_ 25 ppm, using NaCl or CaCl<sub>2</sub> in different  
 163 concentrations of NaCl: 0.02, 0.05, 0.1, and 0.2 mol/L or CaCl<sub>2</sub>: 0.02, 0.05, 0.1 and 0.2 mol/L are  
 164 showed in Figure 4. While using ultrasonic treatment alone cannot remove COD and color of DY7

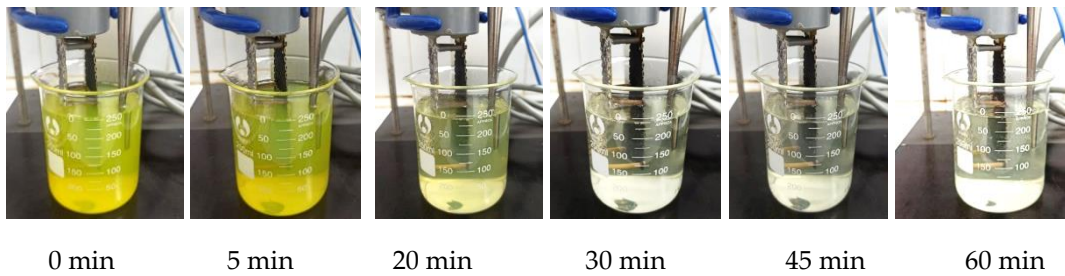
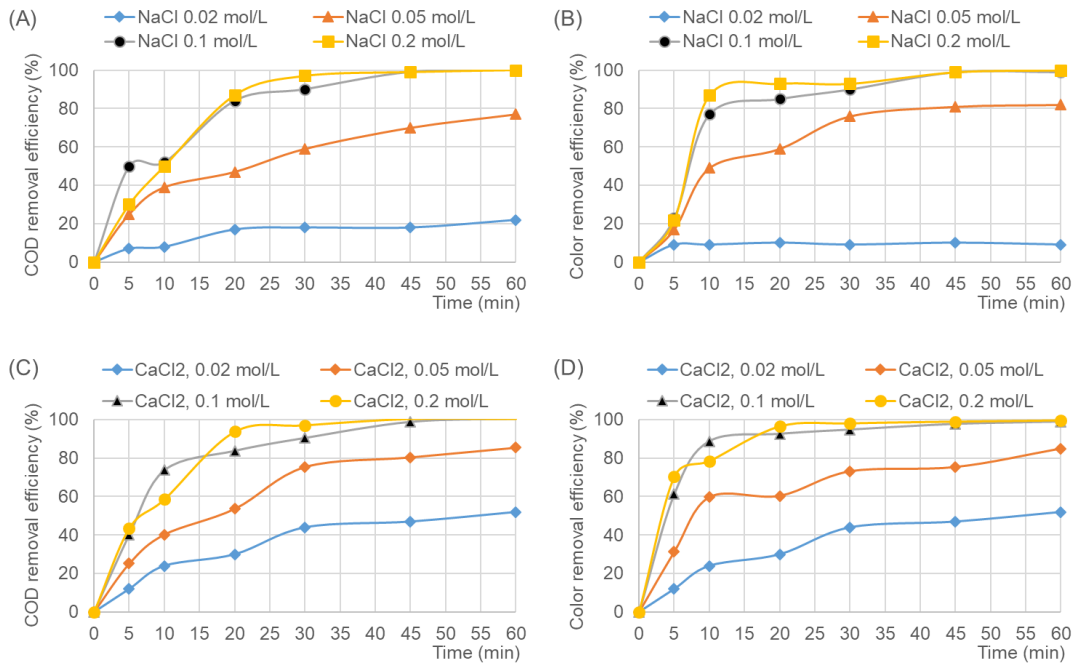
165 solutions (Figure 2). According to the results shown in Figure 3 and Figure 4, it could be  
 166 concluded that the treatment efficiency of combined EC-US is much better under electrolyte using  
 167 (NaCl or CaCl<sub>2</sub>). Interestingly, the combination of EC\_US is performed the highest treatment  
 168 COD and color (DY7\_25 ppm) after 30-mins treatment time with the using of NaCl or CaCl<sub>2</sub> 0.1  
 169 to 0.2 mol/L.



170  
 171 **Figure 3.** Percentage of COD and color removal efficiency in 0.05 mol/L NaCl and 0.05 mol/L  
 172 CaCl<sub>2</sub> during 60 min treatment by EC or EC\_US processes.

173 Changing the concentration of DY7 (10 ppm, 25 ppm, and 50 ppm), and investigating of EC\_US  
 174 treatment these samples, using 0.05 mol/L CaCl<sub>2</sub>, the highest removal efficiency was DY7 10 ppm  
 175 (98%), followed by DY7 25 ppm (85%) and the lowest removal was DY7 50 ppm (72%) after 60  
 176 minutes treatment time. The performance of using EC\_US in the degradation of color and COD  
 177 of dyeing DY7 (10 – 50 ppm) have done in the study. The EC\_US process was totally removal of  
 178 DY7, with the presence removal 100%, after 30 - 60 min treatment time, and much higher than  
 179 the EC process or US process (EC\_US > EC > US). In previous research, Barros et al. (2014) also  
 180 studied the degradation of amaranth dye using an integrated EC\_US technique, with using of a  
 181 fabricated boron-doped diamond thin film as the anode, a platinum net as the cathode, and  
 182 saturated calomel as the reference electrode. The sonolysis was also performed at a frequency of  
 183 20 kHz. It was noted that the EC\_US got a higher degradation efficiency (95%, 90 min) than that  
 184 of EC (80%) or sonolysis (8%) processes alone [6].

185 The current density of the EC process had an important impact on the degradation efficiency [13].  
 186 The effect of wastewater conductivity on dye removal and specific electrical energy consumption,  
 187 various experiments were performed using NaCl as the electrolyte. With an increase in salt  
 188 concentration from 0.1 to 1.0 g/L, a drastic improvement in solution conductivity (from 0.38 to  
 189 1.94 mS) was observed by Nandi, B. K., et al., 2017 [10]. Thus, in this investigation of EC\_US  
 190 processes, there was a significant increase in the electric current (mA) and temperature (°C)  
 191 during the treatment time (from 0 to 60 min). The temperature of all experiments gradually  
 192 increased from 21.5 ± 1.0 °C to 42.0 ± 1.0 °C, and the increase of electric current (mA) after the  
 193 treatment depending on the initial and type of electrolyte (Table 5).



**Figure 4.** Percentage of COD and color removal efficiency (DY7\_25 ppm) by EC\_US processes, using electrolyte NaCl (A, B) or CaCl<sub>2</sub> (C, D), treatment time: 0 – 60 min). Photos of the EC\_US experiment using electrolyte 0.1 mol/L CaCl<sub>2</sub>.

**Table 5.** The electric current (mA) before and after the EC\_US treatment processes.

EC_US process DY7_ 25 ppm	0.02 mol/L NaCl	0.05 mol/L NaCl	0.1 mol/L NaCl	0.2 mol/L NaCl
Electric current (mA) from 0 to 60 min	60 → 60	100 → 150	250 → 320	370 → 470
EC_US process DY7_ 25 ppm	0.05 mol/L CaCl <sub>2</sub>	0.1 mol/L CaCl <sub>2</sub>	0.2 mol/L CaCl <sub>2</sub>	
Electric current (mA) from 0 to 60 min	170 → 230	360 → 440	450 → 530	

#### 4. Conclusions

Performance of using the EC\_US system for color and COD removal from DY7 dyeing water was successfully investigated using supporting electrolytes NaCl and CaCl<sub>2</sub> in different concentrations (0.02, 0.05, 0.1, and 0.2 mol/L). Using only the US treatment process (20 KHz, 500

207 w/cm<sup>2</sup>) was not effective in the treatment of DY7 dye water. However, the combination of EC\_US  
208 is performed the totally removal COD and color (DY7\_25 ppm) after 30-mins treatment time with  
209 the using of NaCl or CaCl<sub>2</sub> 0.1 to 0.2 mol/L, and it could be concluded that the performing of  
210 process EC\_US > EC > US treatment alone. This is the first investigation of using electrolytes CaCl<sub>2</sub>  
211 in EC and EC\_US processes, and interestingly CaCl<sub>2</sub> electrolytes had a higher pigmentation  
212 capacity than NaCl in the same treatment condition. Moreover, after the treatment of the EC\_US  
213 process, the surface of the electrodes used in this study (TiO<sub>2</sub> and RuO<sub>2</sub>-IrO<sub>2</sub>-TiO<sub>2</sub>) is very clean.  
214 According to these results, the EC\_US process could be a valuable alternative to conventional  
215 physicochemical methods for the treatment of textile wastewater and/or other refractory organic  
216 compounds contained in wastewater.

### 217 **Acknowledgments**

218 This research was supported by funding from Hue University (DHH 2021-01-182) and  
219 Huetronics Company Viet Nam.

220

### REFERENCES

- 221 1. Grau P. (1992), Textile industry wastewater treatment, *Water Science and Technology*. 24,  
222 97-103.
- 223 2. Ejder-Korucu M, Gürses A, Dogar C, Sharma S, Acikyildiz M. (2015). Removal of organic  
224 dyes from industrial effluents: an overview of physical and biotechnological applications.  
225 *Green Chemistry for Dyes Removal from Wastewater*. Chapter 1, 1-34.
- 226 3. Lorimer J.P. \*, Mason T.J., Plattes M., Phull S.S. (2000). Dye effluent decolourisation using  
227 ultrasonically assisted electro-oxidation. *Ultrasonics Sonochemistry* 7, 237-242.
- 228 4. Ren YZ, Wu ZL, Franke M, Braeutigam P, Ondruschka B, Comeskey DJ, King PM. (2013).  
229 Sonoelectrochemical degradation of phenol in aqueous solutions. *Ultrasonics sonochemistry*.  
230 20(2), 715-21.
- 231 5. Somayajula A, Asaithambi P, Susree M, Matheswaran M. (2012). Sonoelectrochemical  
232 oxidation for decolorization of Reactive Red 195. *Ultrasonics sonochemistry*. 19(4), 803-11.
- 233 6. Barros WR, Steter JR, Lanza MR, Motheo AJ. (2014). Degradation of amaranth dye in alkaline  
234 medium by ultrasonic cavitation coupled with electrochemical oxidation using a boron-  
235 doped diamond anode. *Electrochimica Acta*. 143, 180-7.
- 236 7. Juliana R. Steter, Willyam R.P. Barros, Marcos R.V. Lanza, Artur J. Motheo. (2014).  
237 Electrochemical and sono-electrochemical processes applied to amaranth dye degradation.  
238 *Chemosphere* 117, 200-207.
- 239 8. Radi MA, Nasirizadeh N, Rohani-Moghadam M, Dehghani M. (2015). The comparison of  
240 sonochemistry, electrochemistry and sonoelectrochemistry techniques on decolorization of  
241 CI Reactive Blue 49. *Ultrasonics sonochemistry*. 27, 609-15.
- 242 9. Yang B, Zuo J, Tang X, Liu F, Yu X, Tang X, Jiang H, Gan L. (2014). Effective ultrasound  
243 electrochemical degradation of methylene blue wastewater using a nanocoated electrode.  
244 *Ultrasonics sonochemistry*. 21(4), 1310-7.
- 245 10. Nandi BK, Patel S. (2017). Effects of operational parameters on the removal of brilliant green  
246 dye from aqueous solutions by electrocoagulation. *Arabian Journal of Chemistry*. 10, 2961-8.
- 247 11. M.D.N.Ramosa, C.S.Santanab, C.C.V.Vellosob, A.H.M.da Silvac, F.Magalhãesd, A.Aguiar.  
248 (2021). A review on the treatment of textile industry effluents through Fenton processes.  
249 *Process Safety and Environmental Protection*. 155, 366-386.
- 250 12. Lucyna B. Kazimierz B., Magdalena F., Marta G., Stanisław L. (2020). Catalytic ozonation of  
251 textile wastewater as a polishing step after industrial scale electrocoagulation. *Journal of*

- 252 *Environmental Management*. 265, 1-11.
- 253 13. Theerthagiri J, Madhavan J, Lee SJ, Choi MY, Ashokkumar M, Pollet BG. (2020).  
254 Sonoelectrochemistry for energy and environmental applications. *Ultrasonics sonochemistry*.  
255 63, 104960.
- 256 14. Yasman Y, Bulatov V, Gridin VV, Agur S, Galil N, Armon R, Schechter I. (2004). A new sono-  
257 electrochemical method for enhanced detoxification of hydrophilic chloroorganic pollutants  
258 in water. *Ultrasonics Sonochemistry*. 11(6), 365-72.
- 259 15. Mardali Yousefpour, Amin Shokuhy. (2012). Electrodeposition of TiO<sub>2</sub>-RuO<sub>2</sub>-IrO<sub>2</sub> coating on  
260 titanium substrate. *Superlattices and Microstructures*. 51, 842 – 853.
- 261 16. APHA. 2005. *Standard methods for the examination of water and wastewater*, 21<sup>st</sup> edition, (APHA)/  
262 (AWWA)/ (WEF), Washington DC, USA.
- 263

## 264 SỬ DỤNG QUÁ TRÌNH SIÊU ÂM-ĐIỆN HÓA ĐỂ LOẠI MÀU 265 VÀ COD CỦA CHẤT NHUỘM MÀU VÀNG PHÂN TÁN 7 266 TRONG DUNG DỊCH 267

268 **Tóm tắt.** Nghiên cứu về hiệu quả sử dụng quá trình siêu âm-điện hóa để loại bỏ màu và COD  
269 (nhu cầu oxy hóa hóa học) của phẩm màu vàng phân tán (DY7, 4 - [4 - (phenylazo) phenylazo]  
270 - o-cresol) trong dung dịch đã được thực hiện ở các nồng độ điện li khác nhau của NaCl và  
271 CaCl<sub>2</sub> (0,02, 0,05, 0,1 và 0,2 mol/L), thời gian xử lý và nồng độ DY7. Sự kết hợp của điện hóa  
272 (EC) và siêu âm (US) được gọi là quá trình siêu âm-điện hóa (EC\_US) cho thấy hiệu quả xử  
273 lý DY7 cao nhất so với việc áp dụng EC hoặc US riêng lẻ (EC\_US > EC > US). Sử dụng điện li  
274 CaCl<sub>2</sub> có khả năng loại màu cao hơn NaCl ở cùng nồng độ. Ở liều DY7: 25 ppm, phương pháp  
275 EC\_US (NaCl hoặc CaCl<sub>2</sub> 0,1-0,2 mol/L, tần số 20 kHz, điện cực TiO<sub>2</sub> và RuO<sub>2</sub>-IrO<sub>2</sub>-TiO<sub>2</sub>) đã  
276 hoàn toàn loại bỏ DY7\_25 ppm trong dung dịch (100% màu sắc và 100% COD) trong vòng 45  
277 phút xử lý. Đây có thể là một phương pháp xử lý thay thế có giá trị áp dụng cho nước thải  
278 nhuộm hoặc các hợp chất hữu cơ khó phân hủy khác có chứa trong nước thải.

279  
280 **Từ khóa:** Siêu âm, điện hóa, siêu âm-điện hóa, Disperse Yellow 7.